

# ME 4555 - Lecture 30 - Bode plots, part II

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let's look at the frequency response of a 2<sup>nd</sup> order system (underdamped):

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \Rightarrow G(j\omega) = \frac{\omega_n^2}{-\omega^2 + \omega_n^2 + 2\zeta\omega \cdot \omega_n j}$$

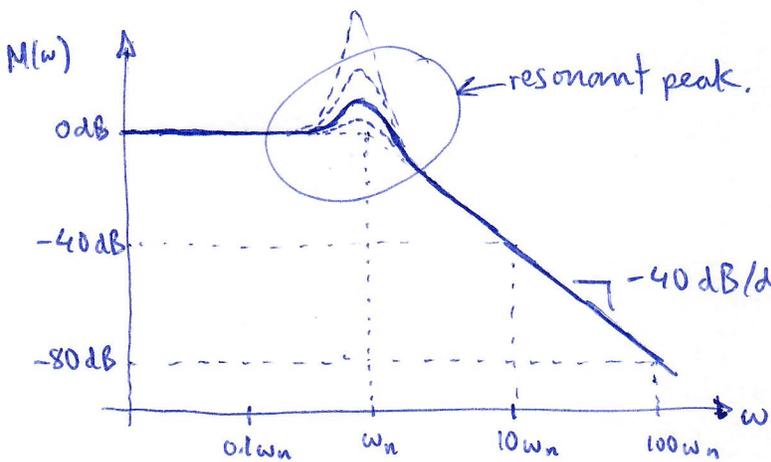
Rewrite as:  $G(j\omega) = \frac{1}{1 - (\frac{\omega}{\omega_n})^2 + 2\zeta(\frac{\omega}{\omega_n})j}$

If  $\omega_n \ll \omega$  (high frequency),  $G(j\omega) \approx -\frac{1}{(\frac{\omega}{\omega_n})^2}$ , therefore,

$$\begin{cases} M_{dB}(\omega) = 20 \log_{10} |G(j\omega)| = -40 \log_{10} (\frac{\omega}{\omega_n}) \quad (\text{slope of } -40 \text{ dB/decade}) \\ \phi(\omega) = -\pi = -180^\circ \quad (\text{since it's a negative number, real}). \end{cases}$$

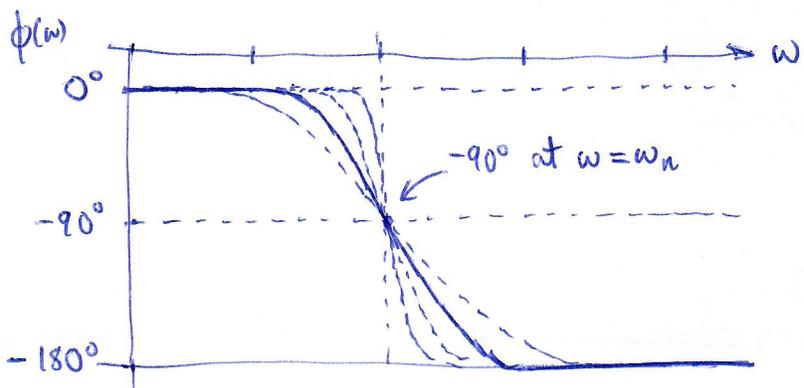
If  $\omega_n \gg \omega$  (low frequency),  $G(j\omega) \approx 1$ , therefore

$M_{dB} = 0 \text{ dB}$ ,  $\phi = 0^\circ$ . (ie. gain of 1). Here is the Bode plot:



for  $\zeta$  closer to zero (less damping), peak is higher.

for  $\zeta \geq \frac{1}{\sqrt{2}} \approx 0.707$ , there is no peak.



for  $\zeta$  closer to zero (less damping), transition is sharper

★ verify this with the interactive demo!

We can derive the properties of the peak in  $M(\omega)$ :

(2)

$$G(j\omega) = \frac{1}{1 - (\frac{\omega}{\omega_n})^2 + 2\zeta(\frac{\omega}{\omega_n})j} \Rightarrow M(\omega) = |G(j\omega)| = \frac{1}{\sqrt{(1 - (\frac{\omega}{\omega_n})^2)^2 + 4\zeta^2(\frac{\omega}{\omega_n})^2}}$$

Peak occurs when  $\frac{d}{d\omega} M(\omega) = 0$ , which is when  $\frac{d}{d\omega} \left[ (1 - (\frac{\omega}{\omega_n})^2)^2 + 4\zeta^2(\frac{\omega}{\omega_n})^2 \right] = 0$

evaluating the derivative + simplifying, this leads to  $4(\frac{\omega}{\omega_n}) \left( (\frac{\omega}{\omega_n})^2 + 2\zeta^2 - 1 \right) = 0$

If  $2\zeta^2 - 1 > 0$ , i.e.  $\zeta \geq \frac{1}{\sqrt{2}}$ , the only solution is  $\omega = 0$ , so there is no resonant peak.

If  $2\zeta^2 - 1 \leq 0$ , i.e.  $0 \leq \zeta < \frac{1}{\sqrt{2}}$ , there is a peak at  $\frac{\omega}{\omega_n} = \sqrt{1 - 2\zeta^2}$

we call this the peak frequency  $\omega_p = \omega_n \sqrt{1 - 2\zeta^2}$

Note that  $\omega_p < \omega_d < \omega_n$ .

$\omega_p = \omega_n \sqrt{1 - 2\zeta^2}$  (peak freq)  
 $\omega_d = \omega_n \sqrt{1 - \zeta^2}$  (damped freq)  
 $\omega_n$  (natural freq).

Peak magnitude is  $M(\omega_p) = \frac{1}{\sqrt{(1 - (1 - 2\zeta^2))^2 + 4\zeta^2(1 - 2\zeta^2)}} = \frac{1}{2\zeta\sqrt{1 - \zeta^2}}$

When  $\zeta$  is small (say  $\zeta < 0.5$ ),  $M(\omega_p) \approx \frac{1}{2\zeta}$ .

So the peak height in dB is  $-20 \log_{10}(2\zeta)$ .

For example, if  $\zeta = 0.05$ ,  $M_{dB}(\omega_p) \approx -20 \log_{10}(0.1) = 20$  dB

if  $\zeta = 0.25$ ,  $M_{dB}(\omega_p) \approx -20 \log_{10}(0.5) \approx 6$  dB.

As  $\zeta \rightarrow 0$ ,  $M(\omega_p) \rightarrow \infty$ .

Both 1<sup>st</sup> and 2<sup>nd</sup> order systems act as low-pass filters

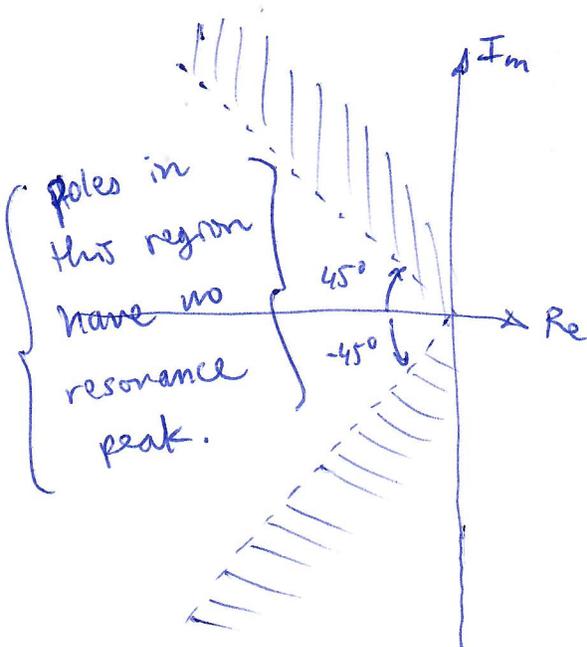
(3)

1<sup>st</sup> order:  $\frac{1}{\tau s + 1} \Rightarrow$  corner at  $\omega_c = \frac{1}{\tau}$ ,  $-20 \text{ dB/decade}$   
for  $\omega \gg \omega_c$ .

2<sup>nd</sup> order:  $\frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2} \Rightarrow$  corner at  $\omega_n$ ,  $-40 \text{ dB/decade}$   
for  $\omega \gg \omega_c$ .

Since  $\zeta < \frac{1}{\sqrt{2}} \approx 0.707$  has a magnitude peak (resonance), it is often desirable to achieve  $\zeta = \frac{1}{\sqrt{2}}$  since it is the least amount of damping required so that there is no peak on the Bode plot.

In the complex plane,  $\zeta = \frac{1}{\sqrt{2}}$  corresponds to a pole angle of  $45^\circ$ .



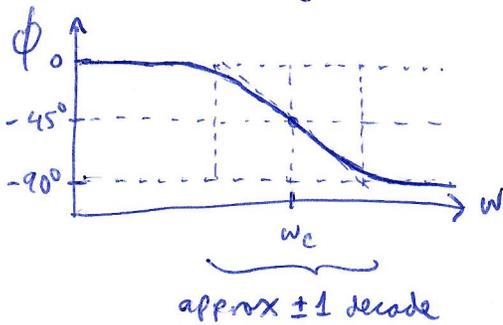
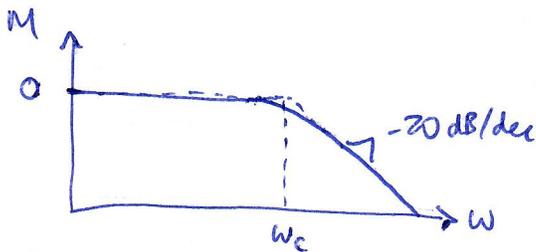
A low-pass filter with  $\zeta = \frac{1}{\sqrt{2}}$  (2<sup>nd</sup> order) is called a Butterworth filter, and it has a transfer function of the form:

$$G(s) = \frac{\omega_n^2}{s^2 + \sqrt{2}\omega_n s + \omega_n^2}$$

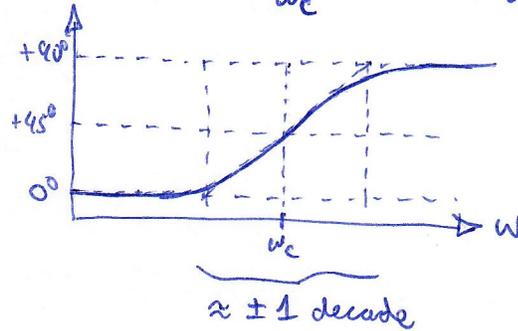
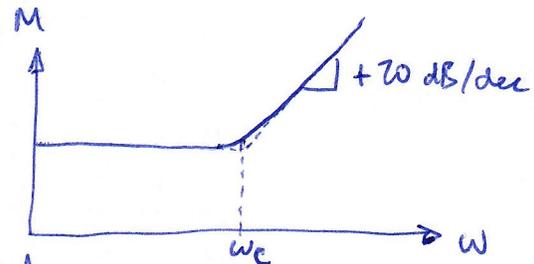
# Sketching Bode plots.

Since magnitude is on a log-scale, we can sketch the Bode plots of each pole + zero separately and just add them up!

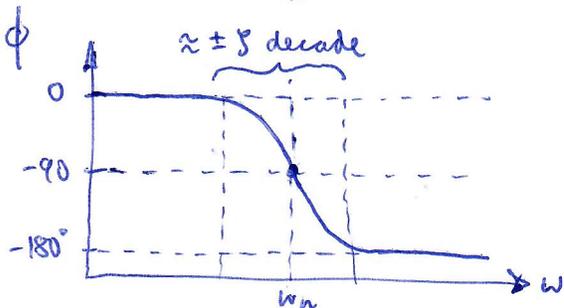
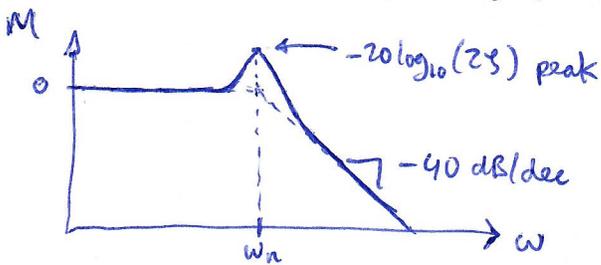
Real pole:  $\frac{1}{\frac{s}{\omega_c} + 1}$



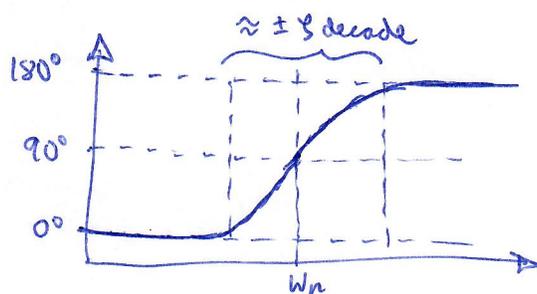
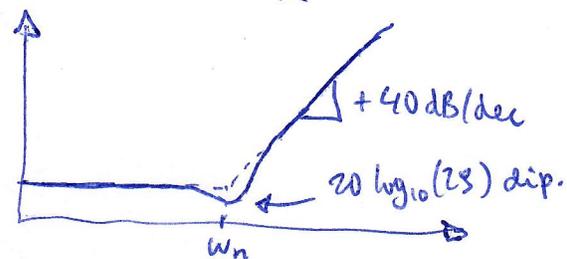
Real zero:  $(\frac{s}{\omega_c} + 1)$



Complex pole:  $\frac{1}{(\frac{s}{\omega_n})^2 + 2\zeta(\frac{s}{\omega_n}) + 1}$



Complex zero:  $[(\frac{s}{\omega_n})^2 + 2\zeta(\frac{s}{\omega_n}) + 1]$



Gain: K.

$M = 20 \log_{10} |K|$

$\phi = 0^\circ$  if  $K > 0$

$180^\circ$  if  $K < 0$

Example  $G(s) = \frac{100(s+1)}{s^2 + 110s + 1000}$  . Sketch the Bode plot. (5)

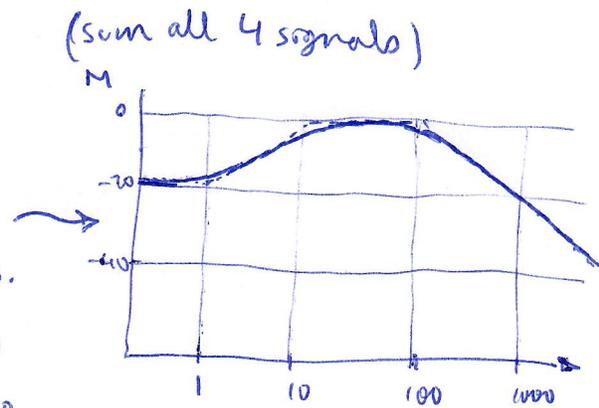
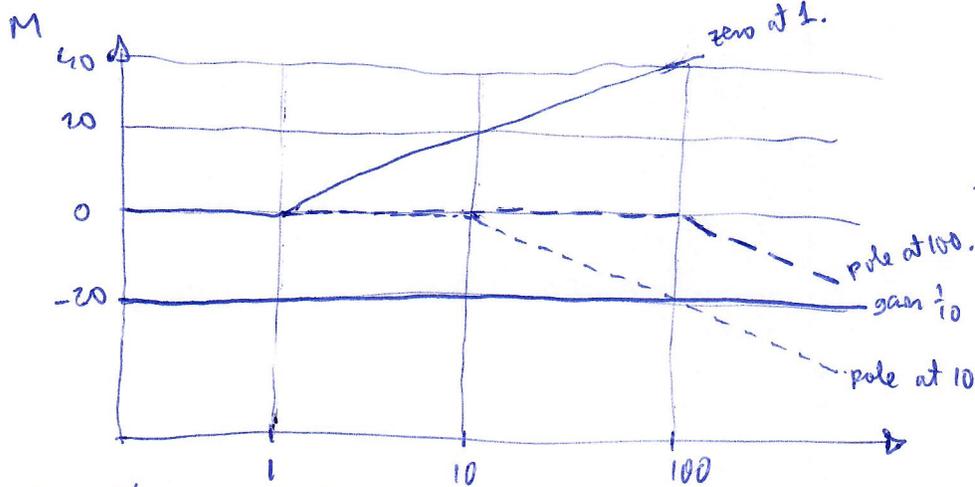
1) put into corner frequency form:

$$G(s) = \frac{100(s+1)}{(s+10)(s+100)} = \frac{1}{10} \cdot \frac{(s+1)}{\left(\frac{s}{10} + 1\right)\left(\frac{s}{100} + 1\right)}$$

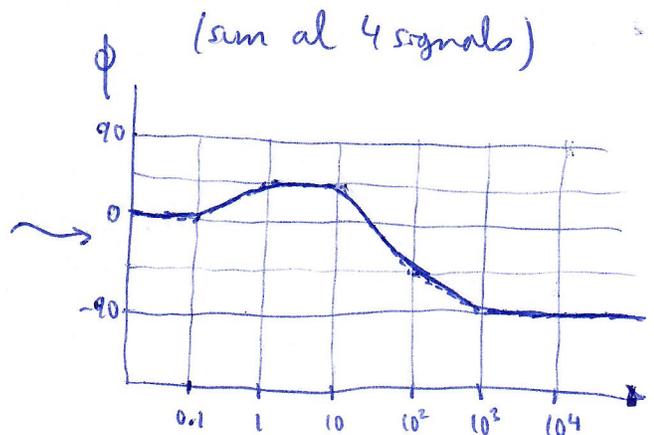
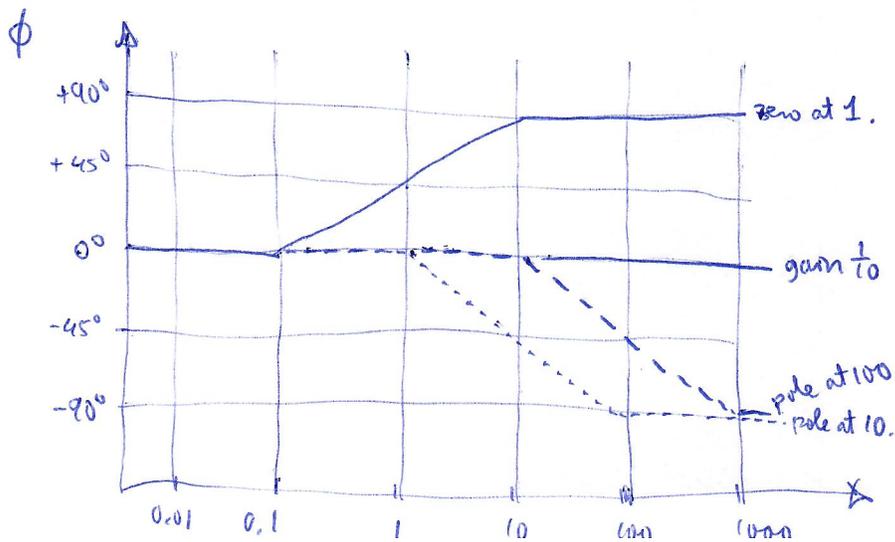
2) decompose: we have:

gain of  $\frac{1}{10}$ , zero at  $\omega_c = 1$ , pole at  $\omega_c = 10$ , pole at  $\omega_c = 100$ .

3) Magnitude plot:



4) Phase plot:

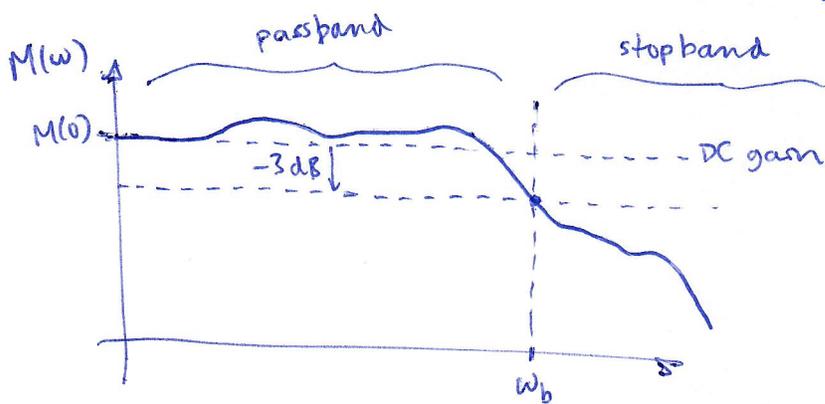


Most real-world systems act roughly like low-pass filters.  
(This is a good thing!)

When  $\omega \rightarrow 0$ , frequency response is  $G(0)$ . Recall this is the same as the steady-state response to a step input by FVT. ↙ DC gain!

When  $\omega \rightarrow \infty$ , once we've exceeded all corner frequencies, the roll-off will occur at a rate of  $-20(n-m)$  dB/decade.  
number of poles minus number of zeros.

The point where the Bode gain plot crosses  $|G(0)| - 3\text{dB}$   
↑ i.e. frequency  
is called the bandwidth ( $\omega_b$ ) of the system.



Why  $-3\text{dB}$ ? because a drop of  $3\text{dB}$  is  $\frac{1}{\sqrt{2}}$  drop in amplitude, i.e.  $\frac{1}{2}$  drop in power. It's where the system attenuates by 50% power.

For a 1<sup>st</sup> order system,  $\omega_b = \omega_c = \frac{1}{\tau}$ .

For a 2<sup>nd</sup> order system,  $\omega_b = \sqrt{1 - 2\zeta^2 + \sqrt{2 - 4\zeta^2 + 4\zeta^4}}$

and when  $0 < \zeta < \frac{1}{\sqrt{2}}$ , we have:  $\omega_p < \omega_d < \omega_n < \omega_b$   
peak      damped      natural      bandwidth

## Summary :

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- a real pole causes a  $-20$  dB/dec roll-off at  $\omega \gg \omega_c$ . ("low pass filter")  
also, a real pole causes  $-90^\circ$  of phase offset (phase lag)
- a real zero causes a  $+20$  dB/dec gain at  $\omega \gg \omega_c$ .  
also, a real zero causes  $+90^\circ$  of phase offset (phase lead).
- a complex pair of poles has the same asymptotic effect as two real poles:  $-40$  dB/dec roll-off and  $-180^\circ$  of phase offset.  
Except there will be a resonant peak of  $\approx -20 \log_{10} 2\zeta$  dB if  $\zeta < \frac{1}{\sqrt{2}}$ . No peak if  $\zeta \geq \frac{1}{\sqrt{2}}$ .
- Same goes for the complex pair of zeros (acts like two real zeros asymptotically).
- Most real-world systems behave like low-pass filters.  
 $\omega_b$  is the frequency where the magnitude drops by 3 dB from the DC gain value (i.e.  $\frac{1}{\sqrt{2}}$  drop in magnitude).  
The pass band is  $\omega < \omega_b$  (frequencies below bandwidth)  
The stop band is  $\omega > \omega_b$  (frequencies above the bandwidth).